

# ATTACHMENT 4 – SERVICING FEASIBILITY ASSESSMENT

Planning Proposal - SP18063 - McMaster (November 2021)

Sept 2021

# Servicing Feasibility Assessment

The logo for MJM Consulting Engineers, featuring the letters 'MJM' in a large, bold, 3D-style font with a metallic or stone-like texture and a slight shadow.

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CIVIL • STRUCTURAL • BUILDING DESIGN • PLANNING

Document Verification Schedule



**Project:**

Airport Street, North Street, Mimosa Street and Bartondale Road, Temora

Servicing Feasibility Assessment

| Revision | Date     | Prepared By   | Checked By  | Approved By  |
|----------|----------|---|---|--|
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## 1. Executive summary

The feasibility of potentially introducing up to six new dwellings within the precinct identified in Figure 1 below was investigated to determine if there was sufficient infrastructure capacity, sewer, stormwater, potable water, electricity, gas and telecommunications to support any proposed development. The current proposal is for an LEP Amendment to reduce minimum lot size from 2ha to 1ha, resulting in a potential introduction of up to an additional six dwellings within the precinct.



Figure 1. Precinct area

In summary the services within the area can cater for up to six additional blocks

| Service       | Summary   | Requires Augmentation to existing system | Ability to service up additional six Blocks |
|---------------|---|--|---|
| Sewer         | The geotechnical report requires min area of 250m <sup>2</sup> for disposal for each dwelling, this area will be easily incorporated into each land parcel therefore the sewer capacity for the additional lots is acceptable.  | No                                       | Yes   |
| Stormwater    | The existing stormwater system will need augmentation with one of the options below<br>1) Upgrade or duplicate the culvert in Airport Street to ensure that the hazard of water on the roadway is kept to at least the status quo or to remove water from crossing in anything other than the 1% AEP.<br>2) Stipulate that all additional dwellings have a discharge equivalent to predeveloped peak discharge from 20% to the 1% AEP | Yes                                      | Yes   |
| Potable Water | There is enough capacity within the network to supply the up to an additional six lots.   | No                                       | Yes   |
| Electricity   | There may need to be augmentation and or upgrades to the existing services to accommodate up to an additional six blocks.   | Yes                                      | Yes   |
| Gas           | The capacity of the existing main will service future and existing block demand<br><br>New mains will need to be installed in Mimosa Street, Bartondale Road and North Street and service lines within Airport Street   | Yes                                      | Yes   |
| NBN           | NBN has identified the area as NBN Fixed wireless.  | No                                       | Yes   |
| Telstra       | Telstra network should not be required due to the area being identified as NBN Fixed wireless   | No                                       | Yes   |

All Services have the ability with some augmentation to supply up to the proposed six additional lots.

## 2. Introduction

This report has been prepared to investigate the feasibility of servicing the up to six additional lots which could result from a proposed amendment to the LEP to reduce the minimum lot size from 2 ha to 1 ha. The report will determine:

- the land capability for effluent systems to service the proposed development.
- the capacity of the Essential Energy network to service the additional lots.
- if there is capacity within the Goldenfields water network and
- options available to facilitate servicing of the proposal.

## 3. Services Capacities

### 3.1 Sewer Capacity

The existing sewer is septic and there is no formal sewer infrastructure within the area. Each lot caters for its own sewer discharge via a bio septic system and an irrigation area or an absorption trench.

It is proposed that the system of disposal of sewer for the additional lots incorporate a similar system as the existing, given this we engaged Aitken Rowe Geotechnical to investigate the site for the capacity for the additional lots and they have recommended for a 4 Bedroom House

|                      |                   |
|----------------------|-------------------|
| Absorption Area      | 250m <sup>2</sup> |
| Or Absorption trench | 192mx 0.6m x 0.7m |

This would easily be incorporated into the proposed 10,000m<sup>2</sup> area.

#### **In summary**

The capacity of the sewer is dependent on the land's capability to accept the produced grey water from the septic systems. It has been shown as above that the area could be incorporated into each land parcel therefore the sewer capacity for the additional lots is acceptable.

Please refer to attached Geotechnical Report attached to this report

### 3.2 Stormwater

There is no formal pipe network for the existing Stormwater within the surrounds of the site.



The site generally falls from Mimosa Street to Airport Street with a gradient of approximately 2%. Mimosa Street is situated on a crest and forms a catchment boundary. The catchment to the west of Mimosa Street falls to Trigalong Creek. The Subject site's main catchment falls from Mimosa Street to Airport Street, Airport Street falls to an existing dam located approx. 200m north of North Street as

shown in the figure below. The outlet of the dam then discharges into the swale in Airport Street and then flows across Airport Street via a small culvert 250m north of North Street as shown in blue below.



*Figure 4. Catchment Plan with outlet – Source Google Earth*



*Figure 5 Small Culvert inlet Airport Street looking south west- source Google earth*



*Figure 6 Small Culvert Outlet on Airport Street looking east- Source Google earth*

The catchment area is approx. 18.7ha. The current culvert will cater for minor flows and larger flows would cross Airport Street approximately at the culvert location. This system is not ideal as it discharges water over Airport Street in a larger storm event which is hazardous to traffic using this street. Adding additional residences will exacerbate the situation, although there are several solutions to improve the situation.

These options are

- 3) Upgrade or duplicate the culvert In Airport Street to ensure that the hazard of water on the roadway is kept to at least the status quo or to remove water from crossing in anything other than the 1% AEP.
- 4) Stipulate that all additional dwellings have a discharge equivalent to predeveloped peak discharge from 20% to the 1% AEP

#### **In summary**

If either of the above-mentioned options are implemented, stormwater system could easily be developed to cater for the future loads.

### **3.3 Potable water**

The existing study area has infrastructure within its surrounds which service the existing lots. The ring main around the development would be able to supply up to an additional six lots according to Goldenfields water. Some augmentation to the system may need to be carried out depending on the layout this would be mainly service conduits to the new lots this may require under-boring of the road.



There is enough capacity within the network to supply the up to an additional six lots.

### 3.4 Electricity

There is existing infrastructure within the surrounds of the site as shown below.

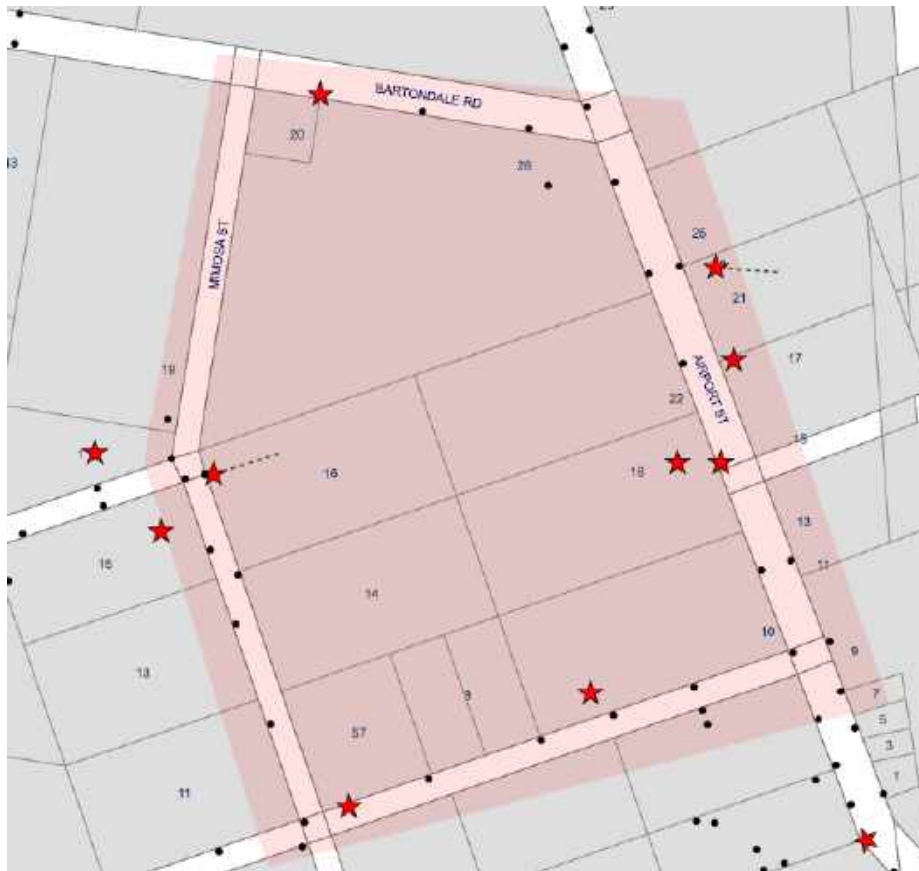


Figure 8 Existing Electrical layout – Source DBYD

MJM consulting engineers contracted David Bridle from DeltaStar designs to access the capacity.

Please find below response from David in relation to existing and capacity and his experience with the area.

*Hi Andrew,*

*It is difficult to tell network capacity without requesting loads from Essential Energy but from the network models I have I can make the following comments (please note that these are not confirmed by Essential Energy and are based on experience with networks and not specific network modelling in this case).*

*Airport Road*

- 1. The HV network along Airport street is a large conductor (7/4.50 AAAC) which is used in urban areas, this line has the potential to support upgrades on this street.*
- 2. The existing substation – Sub 74-318302 along Airport road is already loaded above capacity so would required to be upgraded to support more dwellings*
- 3. The LV network along Airport Street is a large conductor (7/4.50 AAAC) which is used in urban areas, pending the block layout and the location of future lots I would expect this to require upgrade*

*North Street*

1. *The HV Network along North Street is a small conductor (6/1/2.50 ACSR) which is used in more rural areas, as this is a spur it may support upgrades on the network. EE may also request it be brought to a larger conductor to meet load requirements. This would need to be confirmed in a DIP.*
2. *The Existing substation Sub 74-318002 along North Street is at its capacity and would be required to be upgraded to support more dwellings.*
3. *The LV is a mix match of sizes and I am unsure of the open point. I would expect this to be required to be upgraded to an ABC.*

*Mimosa Street*

1. *There is no HV network. Pending the block layout, HV may be required to be run to support a future pole mounted substation*
2. *No Substation is existing. This area is fed from Sub 74-318002 and I would not expect it to meet compliance at any point*
3. *The LV along Mimosa Street is a large conductor (7/4.50 AAAC) but due to its length I do not believe it would be compliant to current standards and a substation would be required on this street to service these blocks.*

*As this land is R5 zoned, Each block would be required to be supplied with 3ph LV.*

*I would recommend obtaining a Feasibility DIP for this site once some form of site plan can be developed. This can be done prior to DA and the DIP need to be reissued once the DA is released.*

*Thanks*

*David*

**In summary**

There may need to be augmentation and or upgrades to the existing services to accommodate up to an additional six blocks.

### 3.5 Gas

The existing study area has infrastructure within its surrounds, notwithstanding this the existing lots are not serviced as indicated in the figure below. MJM have contacted APA (Phil Jenkins by phone 8/10/2021) and he has confirmed the 63dia main running along Airport Street has the capacity to cater for the overall area (existing and proposed). Mains would need to be augmented in North Street, Mimosa Street, Bartondale Road



*Figure 9 Existing Gas layout – Source DBYD*

#### **In summary**

Gas has identified that the capacity of the existing main will service the possible future demand and the existing blocks if they opt to connect.

### 3.6 NBN

The existing site is designated as Fixed wireless as per the figure below



*Figure 10 NBN Service Allocation -Source NBN*

There is existing infrastructure within 520m within the Area which means there would be a possibility of applying for fibre to the kerb because the infrastructure is located within 1km of the site. Please see below figure showing closest location.



*Figure 11 NBN Service Allocation -Source NBN*

### In summary

NBN has identified the area as NBN Fixed wireless.

There is an option to request fibre to the kerb as there are existing services exist within 1km of the site.

### 3.7 Telstra

There is Telstra infrastructure within the bounds of the site as shown in figure 12. The area is designated as fixed wireless by NBN therefore there should be no requirement to augment Telstra Infrastructure

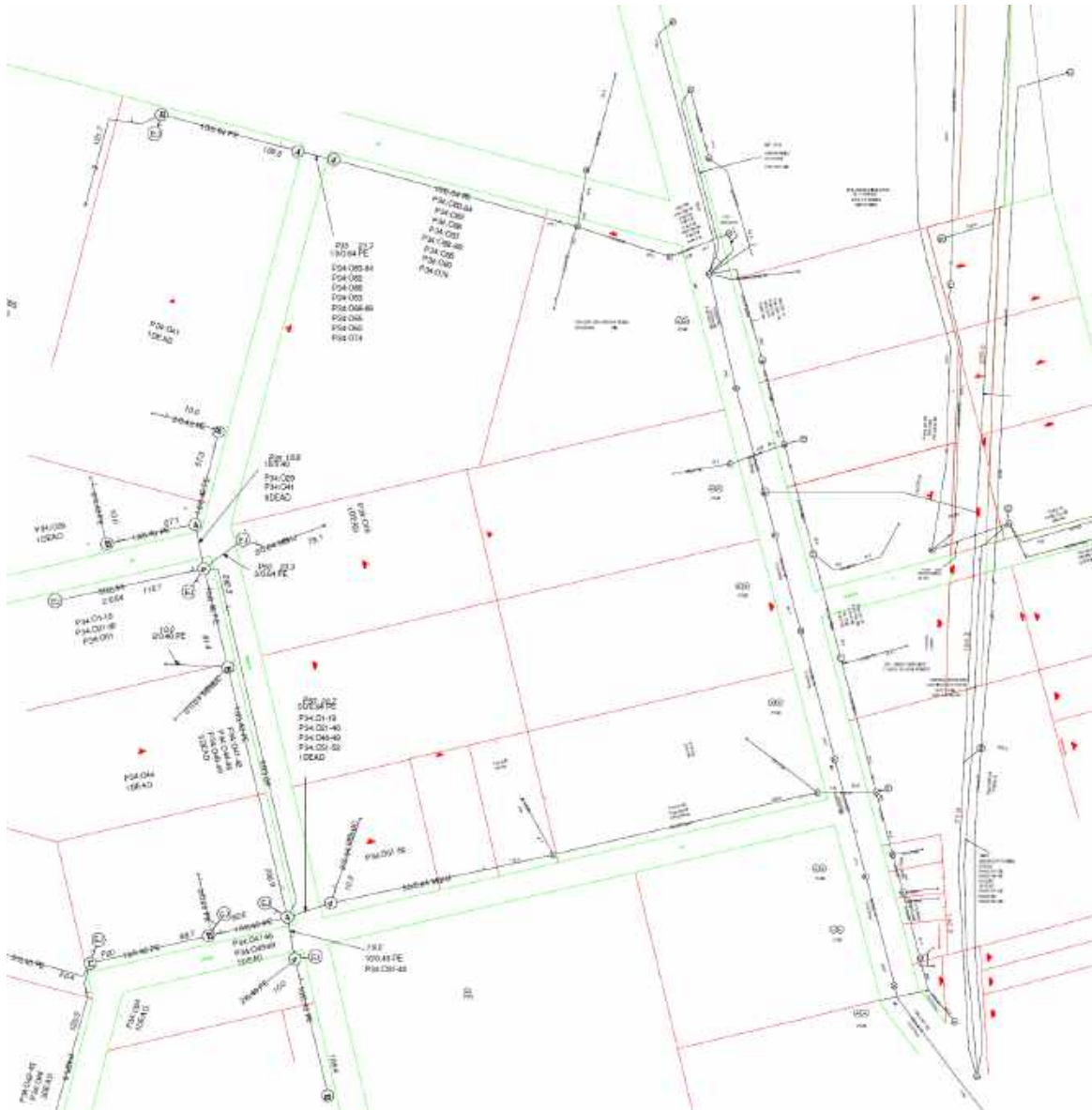


Figure 12 Existing Telstra layout – Source DBYD

### In summary

Telstra network should not be required due to the area being identified as NBN Fixed wireless



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## **Site Assessment For Effluent Disposal System Report**

**CLIENT:** MJM CONSULTING ENGINEERS

**LOCATION:** PROPOSED SUBDIVISION, AIRPORT STREET, TEMORA, NSW

**REGISTRATION No:** ED21-296

**PROJECT DESCRIPTION:** PROPOSED EFFLUENT DISPOSAL SYSTEM

**DATE REQUESTED:** 28 JULY 2021

**DATE OF INVESTIGATION:** 12 AUGUST 2021

**DATE REPORTED:** 15 SEPTEMBER 2021

**ARTL - NATA ACCREDITED LABORATORIES**



## **INTRODUCTION AND PROJECT UNDERSTANDING**

It is the purpose of this investigation to assess the above site for the suitability of an onsite treated effluent disposal system. It is understood that the proposal consists of subdividing the site to allow a further 8 residential dwellings. It should be noted that this is a preliminary investigation to aid in the subdivision process. It is highly recommended to undertake individual investigations for each residential development.

The field investigation including detailed site visit, excavation of a borehole (BH1) to 2.0m and percolation testing were carried out on the 12<sup>th</sup> August 2021. Laboratory testing (Emerson Class and Soil Grading) were completed on recovered samples at our NATA accredited laboratory in Wagga Wagga. A site plan showing borehole/percolation test locations, borehole log and test reports are attached to this report.



## **SITE DESCRIPTION**

The site is located within the township of Temora, New South Wales. The site is situated to the west of Airport Street and is generally flat to slightly undulating.

The borehole investigation revealed the site is underlain by topsoil to 0.1m overlying medium to high & high plasticity clays extending to the borehole termination depth at 2.0m. No groundwater or seepage was encountered during the drilling, however it should be noted that variations to the water table level could fluctuate with changes to the season, temperature and rainfall.

There was no evidence of surface seepage and soaks and the surface soil was moist at the time of the investigation. No sign of erosion was evident and therefore the site should not pose the problem of uncontrolled run-off and erosion. However, run-on and upslope and down slope seepage, if any, to the land application system should be avoided by using earthworks or a drainage system approved by Council.

**Table 1: Land Capability Rating**

| Land Features  |                                   | Land Capability Class Rating |                     |                      |                |                         |             |
|--|-----------------------------------|------------------------------|---------------------|----------------------|----------------|-------------------------|-------------|
|  |                                   | Very Good (1)                | Good (2)            | Fair (3)             | Poor (4)       | Very Poor (5)           | Site Result |
| General Characteristics                                  |                                   |                              |                     |                      |                |                         |             |
| Site drainage / runoff                                   |                                   | Very Slow                    | Slow                | Moderate             | Rapid          | Very Rapid              | 1           |
| Flood / inundation potential (yearly return exceedances) |                                   | Never                        |                     | <1 in 100            | <1 in 20       | >1 in 20                | 1           |
| Slope (%)  |                                   | 0 - 2                        | 2 - 8               | 8 - 12               | 12 - 20        | >20                     | 1           |
| Landslip   |                                   |                              |                     |                      |                | Present or past failure | 1           |
| Seasonal watertable depth (m) (inc perched water tables) |                                   | >5                           | 5 – 2.5             | 2.5 – 2.0            | 2.0 – 1.5      | <1.5                    | 2           |
| Rainfall (mm/yr)   |                                   | <450                         | 450 - 650           | 650 - 750            | 750 - 1000     | >1000                   | 2           |
| Pan Evaporation (mm/yr)                                  |                                   | >1500                        | 1250 - 1500         | 1000 - 1250          | -              | <1000                   | 2           |
| Soil Profile characteristics                             | Structure                         | High                         | Moderate            | Weak                 | Massive        | Single Grained          | 1           |
|  | Profile Depth                     | >2m                          | 1.5 – 2m            | -                    | 1.5m – 1.0m    | <1m                     | 1           |
|  | Percolation (mm/hr)               | 50 - 75                      | 20 – 50<br>75 - 150 | 15 – 20<br>150 - 300 | -<br>300 - 500 | <15<br>>500             | 1-2         |
|  | Stoniness (%)                     | <10                          |                     | 10 - 20              | -              | >20                     | 1           |
|  | Emerson Test (dispersion/slaking) | 5&6                          | 4                   | 3                    | 2              | 1                       | 3-4         |



## FIELD AND LABORATORY RESULTS

The permeability of the underlying clay was assessed by carrying out four series of percolation tests at the site. The tests indicated an average permeability of 0.17m/day on the underlying material. This classifies the underlying soil as “Category 5” as per Table 5.1 AS1547:2012 – “On-site domestic-wastewater management”. A soil grading was performed on the underlying material and confirms the soil to be a “Category 5”. An Emerson Class Test was also performed and indicated the material to be “potentially moderately dispersive”. The percolation, grading and Emerson class test reports are herewith attached. A land capability assessment has also been undertaken in Table 1 above. The results show that the site features range from very good to poor (emerson class) and therefore is considered suitable for primary and secondary treated effluent disposal systems **with appropriate management practices undertaken.**

## Disposal Area Sizing

For the purpose of this preliminary investigation the calculations assume the treated effluent disposal area is to service a 4 bedroom residence that has reticulated water supply. Therefore the calculation rates are based on 150L/person/day (allow 5 persons). This assumption is based on Appendix H in AS1547.

It should be noted that if the above design flow rates are adopted then the minimum design capacity for the septic tank shall be determined by:

- Providing for around 24 hours settling volume plus 8 hours hydraulic buffering volume for the daily flows as adopted.
- Providing for scum and sludge accumulation over a 5 year period using the following rates;
  - 1) All waste ..... 80L/person/year
  - 2) Greywater ..... 40L/person/year
  - 3) Blackwater ..... 50L/person/year

The required disposal area is calculated based on the soil data available for different types of land application system. The following assumptions are made in the calculation:

- Daily effluent flow rate per household - 750 litres\*
- Design Loading Rate (DLR) - 10 mm/day
- Design Irrigation Rate (DIR) - 3mm/day
- Width of the trench (where applicable) - 600mm
- Depth of trench (where applicable) - 700mm
- Depth of aggregate (where applicable) - 300mm
- Depth of topsoil (where applicable) - 300mm
- The underlying materials are assessed to be “potentially non dispersive”.
- “Soil Category 5” as per AS1547
- Climatic data for Wagga Wagga provided by the Bureau of Meteorology is adopted.

Note: \* - Assume 150 litres of waste water per person per day.

### 1. Absorption Trench (Single 4 Bedroom Residence)

Based on the above assumptions, climatic data and water balance analysis undertaken, the following minimum dimensions for the disposal area for the absorption trench disposal system are recommended.

- Minimum Absorption Area (wetted area) - 250m<sup>2</sup>
- Minimum length of the trench - 192m (width 0.6m, depth 0.7m)

## 2. Evapotranspiration – Absorption Area/Trench (Single 4 Bedroom Residence)

Based on the above assumptions, climatic data and water balance analysis undertaken, the following minimum dimensions for the disposal area for the evapotranspiration disposal system are recommended provided that the rate of irrigation does not exceed 3mm/day. **It should be noted that this system is considered suitable for secondary treated effluent only.**

- Area - 180m<sup>2</sup>
- Length - 90m
- Depth of imported material - 200mm

It should be noted that adoption of smaller size disposal area would require deeper depth of imported material. **Vegetation planting on-site to encourage evapotranspiration is considered when calculating irrigation and absorption trench areas for this method of disposal.**

## 3. Pressurised Irrigation System

These systems may be used as alternatives to the conventional sub-surface disposal systems outlined in sections above. Consideration through consultation with the local authority will be required prior to choosing this method of disposal because the treatment system will need to conform to effluent quality standards to ensure protection of public health as such:

- Five days biochemical oxygen demand (BOD5) not greater than 20mg/L
- Suspended solids not greater than 30mg/L
- Thermotolerant coliforms not greater than 10 per 100mL.
- Where chlorine is used as a disinfectant, free residual chlorine measured by a field test at the first irrigation outlet, is not less than 0.5mg/L after a 30min contact period.
- Nutrients not more than authorised by the local authority.

All other requirements are to be met as per AS1547.

## Irrigation Area (Single 4 Bedroom Residence)

Based on the above assumptions, water balance analysis and soil data available, the following minimum irrigation area is recommended provide proper control of the effluent is maintained and the rate of irrigation does not exceed 3mm/day. If planting is to occur on-site then the evapotranspiration method and disposal areas as discussed in section 2 can be adopted provided that the rate of irrigation does not exceed 3mm/day.

- Area - 250m<sup>2</sup>



## COMMENTS AND RECOMMENDATIONS

- This investigation is preliminary only. It is recommended to undertake further works for each individual dwelling.
- Land application shall be placed at least 40m away from any channels and 250m away from any domestic groundwater well.
- The irrigation system can only be used for secondary-treated effluent.
- Primary effluent is normally not suitable for irrigation systems but may be permitted by the local authority under special circumstances.
- The proper drainage system should be incorporated with the land application system design as appropriate to ensure surface run-off does not enter into the system.

Should you have any queries, please do not hesitate to contact us.

Yours truly,

Nathan McLaren  
Environmental Consultant

### Attachments:

- Addendum
- Site Diagram showing Borehole and Percolation Test Locations
- Borehole Logs with Explanatory Note
- Percolation, Emerson Class, and Soil Grading Reports
- Water Balance Calculation

# ADDENDUM



## LIMITS OF INVESTIGATION

The recommendations made in this report are based on the assumption that the test results are representative of the overall subsurface conditions. However, it should be noted that even under optimum circumstances, actual conditions in some parts of the building site may differ from those said to exist, because no geotechnical engineer, no matter how qualified, and no subsurface exploration program, no matter how comprehensive, can reveal all that is hidden by earth, rock and time. Because the investigation procedure generally includes sampling from either one, two or three boreholes, it may not be possible to conclusively establish the presence or extent the condition of the underlying soil and rock over the whole block until site work commences for the construction.

The client should also be aware that our recommendations refer only to our test site locations and the ground level at the time of testing.

The recommendations in this report are based on the following: -

- a) The information gained from our investigation.
- b) The present "state of the art" in testing and design.
- c) The building type and site treatment conveyed to us by the client.
- d) Historical Information

Should the client or their agent have omitted to supply us with the correct relevant information, or make significant changes to the building type and/or building envelope, our report may not take responsibility for any consequences and we reserve the right to make an additional charge if more testing is necessary.

Notwithstanding the recommendations made in this report, we also recommend that whenever footings are close to any excavations or easements, that consideration should be given to deepening the footings.

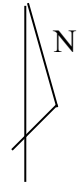
Unless otherwise stated in our commission, any dimensions or slope direction and magnitude should not be used for any building costing calculations and/or positioning. Any sketch supplied should be considered as only an approximate pictorial evidence of our work.



## ADDITIONAL INFORMATION

Refer also to the CSIRO Information Sheet: - BTF18 "Foundation Maintenance and Footing Performance: A Home Owner's Guide, which can be accessed through <http://www.publish.csiro.au/pid/7076.htm>.

# SITE PLAN



NOT DRAWN TO SCALE

## AITKEN ROWE TESTING LABORATORIES PTY LTD

Borehole No.: 1

Sheet No.: 1 of 1

Ground Level: Existing

Date: 12/08/2021

Method: Auger Drilling with TC Bit

GPS N:

E:

| USCS Symbol   | Description   | Depth (m) | Moisture Condition | Consistency/Rel. Density | Sample |     | Lab. Test | Remarks & Field Records        |
|---|---|-----------|--------------------|--------------------------|--------|-----|-----------|--------------------------------|
|   |   |           |                    |                          | Type   | No. |           |                                |
| ML  | TOPSOIL: SILT; low plasticity, brown  |           | MC=PL              | F                        |        |     |           | NATURAL                        |
| CL  | CLAY; low plasticity, trace fine to coarse sand, red brown                            |           | MC>PL              | St.                      |        |     |           |                                |
| CI-CH   | CLAY; medium to high plasticity, trace fine to coarse sand, orange red                | 0.5       |                    | VSt.                     |        |     |           |                                |
|   |   | 1.0       |                    |                          |        |     |           |                                |
| CH  | CLAY; high plasticity, trace fine to coarse sand, trace fine to coarse gravel, orange |           |                    |                          |        |     |           |                                |
|   |   | 1.5       |                    |                          |        |     |           |                                |
| CH  | CLAY; high plasticity, trace fine to coarse sand, mottled cream brown                 |           |                    |                          |        |     |           |                                |
|   |   | 2.0       |                    |                          |        |     |           |                                |
|   | End of Borehole (BH1) @ 2.0m  |           |                    |                          |        |     |           |                                |
|   |   | 2.5       |                    |                          |        |     |           |                                |
|   |   | 3.0       |                    |                          |        |     |           |                                |
|   |   | 3.5       |                    |                          |        |     |           |                                |
|   |   | 4.0       |                    |                          |        |     |           |                                |
| Registration No.: ED21-296                                  |   |           |                    |                          |        |     |           | Logged By: JAG                 |
| Location: Proposed Subdivision, Airport Street, Temora, NSW |   |           |                    |                          |        |     |           | Scale: As shown                |
| Client: MJM Consulting Engineers                            |   |           |                    |                          |        |     |           | Groundwater: Dry on completion |



**AITKEN ROWE TESTING LABORATORIES PTY LTD**  
**LOG SYMBOLS**

| LOG COLUMN                                   | SYMBOLS           |  | DEFINITION  |  |                                |
|--|-------------------|--|---|--|--------------------------------|
| Groundwater Record                           |                   |  | Standing water level. Time delay following completion of drilling may be shown.   |  |                                |
|  |                   |  | Groundwater seepage into borehole or excavation noted during drilling or excavation.  |  |                                |
| Samples                                      | D                 |  | Small disturbed bag sample taken between the depths indicated by lines.   |  |                                |
|  | B                 |  | Bulk disturbed sample taken between the depths indicated by lines.  |  |                                |
|  | U                 |  | Undisturbed 50mm diameter tube sample taken between the depths indicated by lines   |  |                                |
| Field Tests                                  | N=17<br>4, 7, 10  |  | Standard Penetration Test (S.P.T.) performed between depths indicated by lines. Individual figures show blows per 150mm penetration driven by SPT hammer.                         |  |                                |
|  | N <sub>c</sub>    | 5  | Dynamic Cone Penetration Test performed between depths indicated by lines.<br>Individual figures show blows per 100mm penetration for 60 degree solid cone driven by 9 Kg hammer. |  |                                |
|  |                   | 7  |   |  |                                |
|  |                   | 3  |   |  |                                |
| Moisture Condition<br>(Clay or Silt based)   | MC>PL             |  | Moisture content estimated to be greater than plastic limit.  |  |                                |
|  | MC=PL             |  | Moisture content estimated to be approx. equal to plastic limit.  |  |                                |
|  | MC<PL             |  | Moisture content estimated to be less than plastic limit.   |  |                                |
| Moisture Condition<br>(Gravel or Sand based) | D                 |  | DRY – runs freely through fingers.  |  |                                |
|  | M                 |  | MOIST – does not run freely but no free water visible on soil surface.  |  |                                |
|  | W                 |  | WET – free water visible on soil surface.   |  |                                |
| Consistency<br>(Clay or Silt based)          | VS                |  | VERY SOFT – unconfined compressive strength less than 25kPa.  |  |                                |
|  | S                 |  | SOFT – unconfined compressive strength 25-50 kPa.   |  |                                |
|  | F                 |  | FIRM – unconfined compressive strength 50-100kPa.   |  |                                |
|  | St.               |  | STIFF – unconfined compressive strength 100-200kPa.   |  |                                |
|  | VSt.              |  | VERY STIFF – unconfined compressive strength 200 – 400kPa.  |  |                                |
|  | H                 |  | HARD – unconfined compressive strength greater than 400kPa.   |  |                                |
| Relative Density<br>(Gravel or Sand based)   |                   | Description  | Density Index Range %<br>S.P.T.   |  | 'N' Value Range<br>Blows/300mm |
|  | VL                | VERY LOOSE   | <15   |  | 0-4                            |
|  | L                 | LOOSE  | 15-35   |  | 4-10                           |
|  | MD                | MEDIUM DENSE   | 35-65   |  | 10-30                          |
|  | D                 | DENSE  | 65-85   |  | 30-50                          |
|  | VD                | VERY DENSE   | >85   |  | > 50                           |
| Hand Penetrometer Readings                   | 300<br>250<br>280 | Numbers indicate individual test results in kPa on representative undisturbed material unless noted otherwise. |   |  |                                |
| Laboratory Test                              | L.S. %            | Linear Shrinkage (As per RTA Method T113)  |   |  |                                |
|  | M.C. %            | Field Moisture Content (As per Australian Standard AS1289.2.1.1 or RTA Method T120)                            |   |  |                                |
|  | I <sub>ss</sub>   | Shrink-Swell Index (As per Australian Standard AS1289.7.1.1)   |   |  |                                |
| Remarks                                      | 'V' bit           | Hardened steel 'V' shaped bit.   |   |  |                                |
|  | 'TC' bit          | Tungsten Carbide wing bit.   |   |  |                                |
|  | T <sup>60</sup>   | Penetration of auger string in mm under static load of rig rear axle without rotation of augers.               |   |  |                                |

**AITKEN ROWE TESTING LABORATORIES PTY LTD**

ARTL Wagga: 4/2 Riedell Street, Wagga Wagga NSW 2650

PAGE: 1

OF: 1

**TEST REPORT****SOIL PERCOLATION & EMERSON CLASS**

CLIENT: MJM CONSULTING ENGINEERS

PROPERTY LOCATION: EFFLUENT DISPOSAL ASSESSMENT - PROPOSED

SUBDIVISION, AIRPORT STREET, TEMORA, NSW

MATERIAL TYPE: CLAY

DATE OF TEST: 12/08/2021

TEST METHOD: AS1547

AS1289.3.8.1

REGISTRATION No.: **ED21-296****MEASUREMENT OF DROP IN WATER LEVEL**

| Time Elapsed<br>(minutes)    | Water Level (mm) |      |      |      |      |      |
|------------------------------|------------------|------|------|------|------|------|
|                              | P1               | P2   | P3   | P4   | P5   | P6   |
| 0                            | *                | *    | *    | *    | *    | *    |
| 10                           | 8                | 10   | 8    | 10   | 12   | 10   |
| 20                           | 18               | 19   | 16   | 18   | 20   | 19   |
| 30                           | 18               | 28   | 23   | 26   | 27   | 27   |
| 40                           | 23               | 36   | 28   | 33   | 34   | 34   |
| 50                           | 28               | 38   | 30   | 39   | 39   | 37   |
| 60                           | 30               | 40   | 30   | 42   | 42   | 38   |
| Absorption rate<br>mm/25mins | 50.0             | 37.5 | 50.0 | 35.7 | 35.7 | 39.5 |

| Time Elapsed<br>(minutes)    | Water Level (mm) |      |      |      |      |      |
|------------------------------|------------------|------|------|------|------|------|
|                              | P7               | P8   | P9   | P10  | P11  | P12  |
| 0                            | *                | *    | *    | *    | *    | *    |
| 10                           | 15               | 16   | 15   | 25   | 25   | 25   |
| 20                           | 29               | 30   | 30   | 40   | 42   | 40   |
| 30                           | 40               | 40   | 42   | 52   | 55   | 53   |
| 40                           | 44               | 45   | 48   | 67   | 69   | 64   |
| 50                           | 47               | 50   | 52   | 77   | 78   | 70   |
| 60                           | 50               | 52   | 54   | 80   | 81   | 74   |
| Absorption rate<br>mm/25mins | 30.0             | 28.8 | 27.8 | 18.8 | 18.5 | 20.3 |

**Permeability:** 0.17 m/day**D.L.R:** 10 mm/day**D.I.R.:** 3 mm/day**Emerson Class Number:** 2-3

APPROVED SIGNATORY:

  
Nathan McLaren

DATE:

30/8/2021

**AITKEN ROWE Testing Laboratories Pty Ltd**

ARTL Wagga: 4/2 Riedell Street, Wagga Wagga NSW 2650

\*

**TEST REPORT: GEOTECHNICAL INVESTIGATION - SOIL ANALYSIS**

CLIENT : MJM CONSULTING ENGINEERS

JOB DESCRIPTION : EFFLUENT DISPOSAL ASSESSMENT

PROPOSED SUBDIVISION, AIRPORT STREET, TEMORA, NSW

\*

PAGE 1 OF 1

SAMPLED BY: ARTL

DATE SAMPLED: 12/08/2021

DATE SUBMITTED: 12/08/2021

SAMPLING METHOD: \*

SAMPLING CLAUSE: \*

DATES TESTED: 2/09/2021

ORDER No.: \*

MATERIAL SOURCE : IN-SITU BOREHOLES

PROPOSED USE : DESIGN

MATERIAL TYPE : REFER TO BOREHOLE LOGS

REGISTRATION No : R28 **ED21-296**

SAMPLE NUMBER :

P1

P4

P7

P10

\*

\*

SAMPLING LOCATION :

\*

\*

\*

\*

\*

\*

DEPTHS BETWEEN WHICH SAMPLES TAKEN (mm) :

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\*

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TESTS

TEST ELEMENT

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\*

\*

\*

AS1289.3.6.1

PASS 100.0mm SIEVE %

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\*

\*

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\*

\*

PASS 75.0mm SIEVE %

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\*

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\*

\*

PASS 53.0mm SIEVE %

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\*

\*

\*

\*

PASS 37.5mm SIEVE %

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\*

\*

PASS 26.5mm SIEVE %

\*

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\*

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\*

\*

PASS 19.0mm SIEVE %

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\*

\*

\*

\*

PASS 13.2mm SIEVE %

\*

100

\*

100

\*

\*

PASS 9.50mm SIEVE %

\*

95

\*

99

\*

\*

PASS 6.70mm SIEVE %

100

93

100

99

\*

\*

PASS 4.75mm SIEVE %

100

90

99

97

\*

\*

PASS 2.36mm SIEVE %

99

85

97

94

\*

\*

PASS 1.18mm SIEVE %

96

78

93

91

\*

\*

PASS 600µm SIEVE %

63

72

86

89

\*

\*

PASS 425µm SIEVE %

91

70

84

88

\*

\*

PASS 300µm SIEVE %

90

68

82

86

\*

\*

PASS 150µm SIEVE %

87

65

79

83

\*

\*

PASS 75µm SIEVE %

83

61

75

78

\*

\*

AS1289.3.8.1

(AIR DRIED)

EMERSON CLASS

3

2

2

3

\*

\*

TYPE OF WATER

DISTILLED

DISTILLED

DISTILLED

DISTILLED

\*

\*

\*

\*

\*

All samples are oven dried and dry sieved during prep. unless otherwise stated



Accredited for compliance with ISO/IEC 17025 - Testing.

The results of the tests, calibrations and/or measurements included in this document are traceable to Australian/national standards.

ACCREDITATION NUMBER 4679

APPROVED SIGNATORY : .....

DATE: 3/09/2021

Nathan McLaren

SIZE OF AREA FOR EACH MONTH (DISREGARDING STORAGE OF EFFLUENT) 750L/Day

| Month       | Pan Evaporation $E$ mm | Evapotranspiration $ET$ ( $ET=0.75E$ ) | Rainfall $R$ mm | Retained rainfall $R_r$ $R_r = 0.75R$ | $L/TAR$ per Day mm | $L/TAR$ per month mm | Disposal rate per month mm | Effluent applied per month L | Size of Area $m^2$ |
|-------------|------------------------|--|-----------------|---------------------------------------|--------------------|----------------------|----------------------------|------------------------------|--------------------|
| Jan.        | 257.3                  | 193                                    | 43              | 32                                    | 3                  | 93                   | 254                        | 23250                        | 92                 |
| Feb.        | 207.2                  | 155                                    | 37              | 28                                    | 3                  | 84                   | 212                        | 21000                        | 99                 |
| Mar.        | 173.6                  | 130                                    | 42              | 31                                    | 3                  | 93                   | 192                        | 23250                        | 121                |
| Apr.        | 105                    | 79                                     | 46              | 34                                    | 3                  | 90                   | 135                        | 22500                        | 167                |
| May         | 58.9                   | 44                                     | 56              | 42                                    | 3                  | 93                   | 95                         | 23250                        | 244                |
| Jun         | 36                     | 27                                     | 48              | 32                                    | 3                  | 90                   | 85                         | 22500                        | 265                |
| Jul         | 40.3                   | 30                                     | 56              | 42                                    | 3                  | 93                   | 81                         | 23250                        | 287                |
| Aug         | 52.7                   | 40                                     | 54              | 41                                    | 3                  | 93                   | 92                         | 23250                        | 253                |
| Sep         | 75                     | 56                                     | 55              | 41                                    | 3                  | 90                   | 105                        | 22500                        | 214                |
| Oct         | 117.8                  | 88                                     | 62              | 47                                    | 3                  | 93                   | 135                        | 23250                        | 173                |
| Nov         | 177                    | 133                                    | 44              | 33                                    | 3                  | 90                   | 190                        | 22500                        | 119                |
| Dec         | 241.8                  | 181                                    | 42              | 32                                    | 3                  | 93                   | 243                        | 23250                        | 96                 |
| Sum         |                        | 1156.95                                | 584.7           |                                       |                    |                      |                            |                              |                    |
| Ave. Area = |                        |  |                 |                                       |                    |                      |                            |                              | 177                |

DEPTH OF STORED EFFLUENT (TRIAL)

| Month | First Trial area $m^2$ | Effluent applied per month L | Application rate mm | Disposal rate per month mm | Gain/Loss mm | Increase in depth of stored effluent mm | Depth of Effluent for month mm | Increase in depth of effluent mm | Computed depth of Effluent mm |
|-------|------------------------|------------------------------|---------------------|----------------------------|--------------|---|--------------------------------|----------------------------------|-------------------------------|
| Dec.  | 180                    | -                            | -                   | -                          | -            | -                                       | -                              | -                                | 0                             |
| Jan.  | 180                    | 23250                        | 129                 | 254                        | -125         | -415                                    | 0                              | -415                             | -415                          |
| Feb.  | 180                    | 23250                        | 129                 | 212                        | -82          | -275                                    | -415                           | -275                             | -690                          |
| Mar.  | 180                    | 23250                        | 129                 | 192                        | -63          | -210                                    | -690                           | -210                             | -900                          |
| Apr.  | 180                    | 23250                        | 129                 | 135                        | -5           | -18                                     | -900                           | -18                              | -918                          |
| May   | 180                    | 23250                        | 129                 | 95                         | 34           | 114                                     | -918                           | 114                              | -804                          |
| Jun   | 180                    | 23250                        | 129                 | 85                         | 44           | 147                                     | -804                           | 147                              | -657                          |
| Jul   | 180                    | 23250                        | 129                 | 81                         | 48           | 160                                     | -657                           | 160                              | -496                          |
| Aug   | 180                    | 23250                        | 129                 | 92                         | 37           | 125                                     | -496                           | 125                              | -372                          |
| Sep   | 180                    | 23250                        | 129                 | 105                        | 24           | 81                                      | -372                           | 81                               | -291                          |
| Oct   | 180                    | 23250                        | 129                 | 135                        | -6           | -18                                     | -291                           | -18                              | -310                          |
| Nov   | 180                    | 23250                        | 129                 | 190                        | -61          | -202                                    | -310                           | -202                             | -512                          |
| Dec   | 180                    | 23250                        | 129                 | 243                        | -114         | -379                                    | -512                           | -379                             | -891                          |

**CALCULATION OF IRRIGATION AREA**

Area  $A_i = Q_w / DLR$

$Q_w = 5250 \text{ Litre}$

$DLR = 21 \text{ mm/week}$

$DLR = \text{design irrigation rate}$

**Irrigation  $A = 250 \text{ m}^2$**

**CALCULATION OF ABSORPTION TRENCH**

**Data**

width  $b = 750 \text{ mm}$

depth  $d = 700 \text{ mm}$

aggregate depth  $= 300 \text{ mm}$

Note:

$b = \text{minimum } 200 \text{ mm, max. } 750 \text{ mm, Typical } 300\text{-}450 \text{ mm}$

Depth of aggregate  $= \text{min. } 200 \text{ mm, max. } 400 \text{ mm, Typical } 200\text{-}400 \text{ mm}$

Depth of topsoil  $= \text{min. } 100 \text{ mm, max. } 150 \text{ mm, Typical } 100\text{-}150 \text{ mm}$

$A_w = \text{wetted area}$

$Q_d = \text{design daily flow in L/Day}$

$Q_d = 750 \text{ litre}$

$DLR = \text{Design Loading Rate in mm/d}$   
 $DLR(\text{Primary}) = 5 \text{ mm/day}$   
 $DLR(\text{Secondary}) = 8 \text{ mm/day}$

$W = \text{width in mm}$

$A_w = Q_d / L \cdot TAR$

$Q_d = 750 \text{ litre}$

$L \cdot TAR =$

$3 \text{ mm/day}$

$L \cdot TAR = \text{Long Term Acceptance Rate (mm/day)}$

**$A_w = 250 \text{ m}^2$**

$L = A_w / b + d_w$

$L = \text{trench length (m)}$

$A_w = \text{wetted area}$

$b = \text{trench width}$

$d_w = \text{allowance for depth of wetted walls (m)}$

**Length,  $L = 192 \text{ m}$**

$L = Q_d / DLR \cdot W$

$L = \text{length in mm}$

**Length,  $L = 214 \text{ m (for primary effluent)}$**

**$L =$**

**$134 \text{ m (for secondary effluent)}$**

**CALCULATION OF EVAPOTRANSPIRATION - ABSORPTION AREA/TRENCH**

Area,  $A_e = 180 \text{ m}^2$

$Be = \text{width} + 2 \cdot \text{depth}$

Length,  $L = A_e / Be$

**Length,  $L = 90 \text{ m}$**